

JUNCTION SYSTEM AND PROCEDURE FOR JOINING JOINT ASSEMBLY FOR
CONNECTING A FILIFORM ELEMENT TO A CONNECTION ELEMENT

SPECIFICATION

CROSS REFERENCE TO RELATED APPLICATIONS

5 This application is the US national phase of PCT
application PCT/EP2004/005540, filed 24 May 2004, published 09
December 2004 as WO 2004/106772, and claiming the priority of
Italian patent application MI2003A001065 itself filed 28 May
2003, whose entire disclosures are herewith incorporated by
10 reference.

FIELD OF THE INVENTION

The present invention refers to a junction system for
joining connecting a tensile stress-resistant filiform element to
a connection element.

15 BACKGROUND OF THE INVENTION

For some time cables used in multiple applications have
been present on the market, for example for furnishing the
support rigging for the mast of sailboats, or for the support of
poles, or for the pretensioning of beams which must support a
20 bending torque, or for still other structures.

Such cables must possess an adequate resistance to
tensile stress, thus they are usually made [[in]] of metallic
material and in particular in steel. Furthermore, such cables
must be ~~fastened to~~ secured at their ends, for example in a
25 sailboat one ~~end of the head~~ outer end is connected to the ~~summit~~

top of the mast, and the other end to a connector fastened on the bridge.

Such cables notoriously present several drawbacks, including the fact that the constituent materials have an elevated density and an excessive overall weight for some applications. For example, the weight of the cable which maintains the sailboat mast must be balanced by an additional weight applied to the boat keel. Since the lever arm of the moment exercised by the weight applied to the mast is considerably ~~[[above]]~~ greater than the lever arm of the moment exercised by the weight applied to the keel, the value of the additional weight applied to the keel must be considerably above the weight applied to the mast. Naturally, this perversely affects boat stability and performance.

Another drawback of traditional cables consists in the fact that the ~~extremities~~ ends are damaged by wear and tear, continuous rubbing, impact, and shearing both by atmospheric agents and by the elements to which they are connected.

Still another drawback of traditional cables is due to the use of extremely expensive materials in order to confer optimal properties of resistance to tensile stress and stiffness.

A further drawback of traditional cables is due to the use of a generally complex ~~system of junction~~ joint assembly to a connection element, which may be installed only by highly specialized personnel.

Finally, such traditional cables have the drawback of generating, due to their generally circular-section shape, an increased aerodynamic resistance independent ~~[[from]]~~ of the direction of the fluid which impacts it.

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OBJECT OF THE INVENTION

The ~~technical task which~~ object the present invention proposes is, therefore, ~~that of achieving~~ to provide a junction system for ~~joining~~ connecting a tensile stress-resistant filiform element to a connection element ~~which~~ that permits the
10 elimination of the above-mentioned technical drawbacks of the known technique.

~~Within the scope of this technical task one~~ Another object of the invention is to ~~achieve~~ provide a junction system for ~~joining~~ connecting a tensile stress-resistant filiform
15 element to a connection element ~~, in which~~ where the filiform element has a low density but notable properties of resistance to tensile stress and stiffness ~~[[,]]~~ such that it has an extremely limited overall weight, ideal for many applications.

Another object of the present invention is to supply a
20 junction system for ~~joining~~ connecting a tensile stress-resistant filiform element to a connection element ~~which has a protection~~ of that protects the filiform element against damage by wear and tear, continuous rubbing, impact, and shearing both by atmospheric agents and by the elements to which they are
25 connected.

Another object of the present invention is to supply a junction system for joining connecting a tensile stress-resistant filiform element to a connection element, in which the filiform element has ideal properties of resistance to tensile stress and stiffness even if ~~being achieved in an economical~~ while being made of inexpensive material.

A further object of the present invention is to ~~achieve~~ provide an easy-to-install junction system for joining connecting a tensile stress-resistant filiform element to a connection element, even by personnel that are not ~~highly~~ specialized personnel.

Last but not least an object of the present invention is to ~~present~~ provide a device for reducing the aerodynamic resistance of a tensile stress-resistant filiform element subject to a fluid flux flow of variable direction.

SUMMARY OF THE INVENTION

The technical task, as well as these and other objects according to the present invention, are achieved by making a junction system for joining connecting a filiform element to a connection element, characterized ~~in that having by~~ by a tubular ~~element tube~~ fitted on an end section of ~~said the~~ filiform element and substantially having an eye for ~~hooking said into~~ which the connection element can be hooked.

According to a further aspect of the present invention, a procedure for ~~achieving a system of junction of~~ making such a joint assembly between a filiform element ~~and~~ and a connection

element is ~~revealed~~, characterized in that a ~~tubular element tube~~ is fitted on an end section of ~~said the~~ filiform element, and [[said]] ~~this tubular element tube~~ is shaped such that it ~~determines forms~~ an eye adapted to ~~be hooked by the~~ [[said]] connection element.

According to a third aspect of the present invention, a method (and a device) for reducing the aerodynamic resistance of a filiform element subject to a fluid ~~flux~~ flow of variable direction is ~~revealed~~, characterized for the ~~application mounting~~ of a highly aerodynamic wing profile along at least one section of ~~said the~~ filiform element, supported and freely rotating around ~~said the~~ filiform element such that it orients itself in the direction of the fluid ~~flux~~ flow ~~which that~~ impacts it. ~~Other characteristics of the present invention are defined,~~ moreover, in subsequent claims.

BRIEF DESCRIPTION OF THE DRAWING

Further characteristics and advantages of the invention shall be more evident from the description of a preferred but not exclusive embodiment of the junction system according to the ~~finding invention~~, illustrated as significant and non-limiting in the attached drawings, in which: [[-]]

figure FIG. 1 shows a section ~~ed view of through~~ a first preferred embodiment of the junction system according to the present ~~finding invention~~; [[-]]

figure FIG. 2 shows a ~~sectioned view of through~~ a device for reducing ~~[[the]]~~ aerodynamic resistance according to the present finding invention; ~~[[-]]~~

figure FIG. 3 shows an ~~elevated side view of an axial~~ ~~[[ly-]]~~ section ~~[[ed]]~~ through a second preferred embodiment of the junction system according to the present finding invention; and ~~[[-]]~~

figure FIG. 4 shows an ~~elevated side view of an axial~~ ~~[[ly-]]~~ section ~~[[ed]]~~ through a third preferred embodiment of the junction system according to the present finding invention.

Equivalent parts in the description will be indicated by the same reference number.

SPECIFIC DESCRIPTION

With reference to figure FIG. 1, a junction system 1 is shown for joining connecting a filiform element 2 to a connection element (not shown). The junction system 1 has a ~~tubular element~~ tube 3 fitted on an end section of the filiform element 2 and substantially defining an eye 4 ~~into which the connection element can be hooked~~. In this embodiment, the ~~tubular element~~ tube 3 and the eye 4 are made in a single piece.

The ~~tubular element~~ tube 3 has a curved section 5 defining the eye 4, and at least a first substantially straight section 6 distal from the ~~[[head]]~~ outer end 7 of the end section of the filiform element 2. At least the first straight section 6 of the ~~tubular element~~ tube 3 may be ~~[[bound]]~~ bonded to the filiform element 2, for example by ~~way of~~ an adhesive. The first

straight section 6 of the ~~tubular element~~ tube 3 has a predetermined length such that the tensile stress force is at least partially or completely transferred from the filiform element 2 to the ~~tubular element~~ tube 3, corresponding exactly with the first straight section 6 of the ~~tubular element~~ tube 3. The first straight section 6 of the ~~tubular element~~ tube 3 may be extended, also simply for protecting the filiform element 2 ~~placed in its interior inside it~~. The ~~tubular element~~ tube 3 has flared ends ~~edges~~, in order to avoid transversely cutting the filiform element 2.

Preferably, the ~~tubular element~~ tube 3 then presents also has a second substantially straight section 8, proximal to the ~~[[head]]~~ outer end 7 of the end section of the filiform element 2. Preferably, the filiform element 2 may be of composite material, for example ~~[[in]]~~ a continuous longitudinal fiber having a thermoplastic resin matrix, while the ~~tubular element~~ tube 3, may be ~~[[in]]~~ of steel if there are no corrosion problems, stainless steel if there are corrosion problems, or also ~~[[in]]~~ of another metallic material or in plastic in other applications.

When increased mechanical strength properties are required, the fibers of the composite material may be of carbon, aramide, S glass or PBO. Otherwise, for reasons of economy and where lower mechanical properties are required, glass fibers may be employed. It may be advantageous to combine different composite materials to make the filiform element 2, for example

an internal composite material of carbon fibers to confer the desired stiffness and an external composite material in aramide to confer resistance to abrasion. The thermoplastic matrix may be made ~~[[in]]~~ of TPU, nylon, PEEK or polypropylene.

5 The filiform element 2 may be ~~presented in the form of~~
a composite round bar strand, or a plurality of composite round
bar strands, aligned or intertwined among themselves. The
resinous matrix of the constituent composite of the filiform
element 2 may alternatively be of thermosetting type. If the
10 round bar strands are not of circular ~~transversal~~ cross section,
they may be assembled such that they give rise to a substantially
circular configuration. The filiform element 2 may also be
~~presented in~~ of plastic or metal, for example steel, where weight
is not a critical factor in the application. The facing surfaces
15 of the ~~tubular element~~ tube 3 and the filiform element 2 may
define ~~[[the]]~~ spaces specifically made to contain the adhesive
material.

 The filiform element 2 may have a protective coating
(not shown) against ultraviolet rays and/or against attacks of
20 chemical nature and/or against damage of mechanical origin. The
filiform element 2 and/or its protective coating may additionally
have both a predetermined coloration for identifying the diameter
of the filiform element 2 and/or for visually indicating the
filiform element 2, and length markers for facilitating the
25 measurement of the filiform element 2 during the making of the
junction system. The junction system has means ~~[[of]]~~ for

locking the eye 4 ~~closing~~ closed, in particular formed by a ring 10 applied around the neck of the eye 4.

The procedure for making a system of ~~junction of~~ for joining connecting the filiform element 2 to a connection element foresees fitting the ~~tubular element~~ tube 3 on the end section of the filiform element 2, and ~~[[to]]~~ forming the ~~tubular element~~ tube 3 such that it defines the eye 4. In such a procedure, ~~as said,~~ the filiform element 2 may be ~~bound~~ bonded to the ~~tubular element~~ tube 3 in order to more efficiently transfer the tensile stress load from one to the other. The bond, as ~~[[seen]]~~ shown, may be ~~achieved~~ made with an adhesive applied to the outer surface of the filiform element 2 before the introduction of ~~this last it~~ into the ~~tubular element~~ tube 3, or by applying a low-viscosity adhesive on the interface between the filiform element 2 and the ~~tubular element~~ tube 3 after the ~~molding of these last~~ forming them, the adhesive penetrating by capillarity or by applying a vacuum or pressure at an end of the ~~tubular element~~ tube 3.

Alternatively, if the filiform element 2 is of composite thermoplastic material, the bond may ~~derive from the~~ be formed by at least partial melting of the resinous matrix of the composite material ~~[[which]]~~ so it adheres to the inner surface of the ~~tubular element~~ tube 3.

Naturally, the length required for the transfer of the load from the filiform element 2 to the ~~tubular element~~ tube 3 depends on a plurality of factors including, among others, the

quality of the interface and the properties of the adhesive. A tighter contact at the interface and/or a higher adhesion coefficient reduces the transfer length.

To make a ~~system of junction~~ joint assembly of the
5 filiform element 2 ~~[[in]]~~ of thermoplastic composite material to the connection element, a kit comprising a folding bending device (not shown) for the ~~tubular element~~ tube 3 will suffice, having means ~~[[of]]~~ for heating adapted to simultaneously heat the filiform element 2 and the ~~tubular element~~ tube 3 to a
10 predetermined temperature at which the filiform element 2 and the ~~tubular element~~ tube 3 become malleable, to be shaped such that they substantially define the eye 4.

Optionally, the heating and the folding bending of the filiform element 2 and the ~~tubular element~~ tube 3 may be
15 undertaken by especially dedicated devices. For example, the heating may be executed by a hot air pistol, by an oven, by heated metallic plates etc. while the folding bending may be achieved by a traditional bending machine. Naturally, if the resinous matrix of the composite is thermosetting, the folding
20 bending is executed at cool temperatures.

One particular junction procedure is described below
[[.]] :

The filiform element 2 is a ~~bar with~~ strand of 5 mm diameter and 1,000 mm length, made ~~[[in]]~~ of a thermoplastic
25 composite material of carbon fiber embedded in an ETPU matrix.

The ~~tubular element~~ tube is a stainless steel tube of 300 mm length.

The end 200 mm of the tube is heated to 160°C.

5 The tube and the ~~bar in its interior~~ strand inside it are ~~folded~~ bent such that they form a hooking eye; they are then cooled.

Two stainless steel rings ~~[[of]]~~ 10 mm ~~length~~ long are flattened such that they assume an oval shape, and the end of the not-yet-shaped ~~bar~~ strand is inserted in them.

10 The end of the not-yet-shaped ~~bar~~ strand is inserted into a second stainless steel tube ~~[[of]]~~ 300 mm ~~length~~ long, after which the other end of the ~~bar~~ strand is shaped in order to form the second hooking eye.

Each ring is seamed at the neck by a corresponding eye.

15 Finally, each eye is hooked to a corresponding connection element.

With reference now to ~~figure~~ FIG. 3, the junction system 1 has removable connection means 100 between the ~~tubular element~~ tube 3 and the eye 4. Such connection means of
20 ~~connection~~ comprise a threaded stem 101 ~~[[which]]~~ that extends from the eye 4 and screws into a first end 102 of the ~~tubular element~~ tube 3.

25 The junction system 1 has an ~~anti-unthreading~~ retaining element 103 adapted to prevent the ~~unthreading of~~ the filiform element 2 from pulling out of a second end 104 of the ~~tubular element~~ tube 3. The ~~anti-unthreading~~ retaining element 103

consists of a pin inserted axially ~~into~~ correspondence with the end of the filiform element 2 positioned in the ~~tubular element tube~~ 3, and has a maximum cross section greater than the inner clearance of the ~~tubular element tube~~ 3. In a preferred form, the pin 103 has a conical or frustoconical shape, in order to facilitate ~~[[the]]~~ centering with respect to the generally cylindrical filiform element 2, and to obtain a homogenous deformation of the filiform element 2 during ~~[[the]]~~ penetration.

The filiform element 2 is preferably of thermoplastic composite material, directly or indirectly heatable to a softening temperature adapted to permit ~~[[the]]~~ penetration of the pin. The filiform element 2 ~~softening~~ may be obtained softened by an external heat source applied directly to it, or by ~~[[the]]~~ friction ~~which is~~ generated during pin penetration, or by heating the pin first and/or during its insertion, or by heating the ~~tubular element tube~~ first and/or during pin insertion.

In the junction system 1 now illustrated the filiform element 2 is axially hollow in order to facilitate the pin penetration. The filiform element 2 may more generally ~~have full~~ be solid or of empty or hollow section in order to be lighter.

With reference now to ~~figure~~ FIG. 4, the junction system 1 ~~presents the~~ has an eye 4 formed in a single piece ~~[[,]]~~ with the ~~tubular element tube~~ and the means ~~[[of]]~~ for screw connection 105 being between the inner ~~[[side]]~~ surface of the ~~tubular element tube~~ 3 and the outer ~~[[side]]~~ surface of the end section of the filiform element 1. At least ~~in correspondence~~

with the zone at the region of engagement between the thread
[[ing]] of the filiform element 2 and the counter-thread [[ing]]
of the tubular element tube 3 which that defines [[such]] this
screw connection means, an axial ~~discharge~~ void 106 [[of]] in the
5 filiform element 2 ~~is foreseen which~~ being provided that permits
~~this last a~~ it to radially deform [[ation]] . Preferably, in
fact, the thread [[ing]] of the filiform element 2 is preferably
~~obtained~~ formed by inserting a pin in the axial ~~discharge~~ void
106 in order to radially push the filiform element 2 from the
10 inside toward the outside against the wall of a mold having the
impression shape of the thread [[ing]].

The filiform element 2 of the above-discussed
embodiments ~~illustrated until now~~ may be constituted in its
entirety by ~~poltruded~~ extruded longitudinal fibers. Nevertheless
15 it is equally conceivable that the filiform element 2 has a first
section in ~~poltruded~~ extruded longitudinal fiber [[,]] comprising
the end section on which the tubular element tube 3 is fitted
[[,]] and a second section extending from the first section in
free or intertwined non-~~poltruded~~ extruded longitudinal fibers.

20 According to another aspect, the present invention
~~reveals~~ includes a method for reducing the aerodynamic resistance
of a filiform element subject to a fluid flux flow of variable
direction. Such method foresees the application of an element of
wing profile along at least a section of the filiform element,
25 supported and freely rotating around the filiform element such

that it orients itself in the direction of the fluid ~~flux~~ flow that impacts it.

An element with highly aerodynamic wing profile is illustrated in ~~figure~~ FIG. 2, which as an example makes reference to a shroud 30, in particular in composite material, which may be used to ~~reinforce~~ brace the vertical mast of a sailboat.

As known, the aerodynamic resistance D of a body struck by a fluid ~~flux~~ flow is expressible as: $D = C_x \times L \times W \times V^2$ where C_x is a ~~coefficient which accounts for~~ factor related by the body shape, L is the length of the body, W is the diameter of the body, and V is the relative velocity between the body and the fluid. It should be noted that with L, W and V ~~equivalent~~ the same the wing profile of the aerodynamic element here illustrated has a C_x substantially equal to half that of the circular section of the shroud.

The element with highly aerodynamic profile is constituted by a wing-shaped foil 31 having elastically ~~pliable~~ deformable opposing edges 32 for the snap-lock introduction of the shroud 30. The foil 31 is made from a plastic extrusion, preferably colored so that it ~~results easily~~ is highly visible. The foil 31 also has ~~additionally~~ at least a first extension, in particular two extensions 33, jutting out from its inner surface to join the foil 31 to a precise point on the longitudinal length of the shroud.

Possibly, the foil 31 may have a plurality of extensions (not shown) jutting out from the inner surface, for

example angularly-spaced and radially-oriented with respect to the shroud 30, in order to join the foil 31 to a precise point on the longitudinal length of the shroud 30 having a substantially smaller diameter than that of the maximum chord of the curved
5 part of the foil 31. In such a manner the foil also operates as an element of protection of the shroud from accidental impact.

The junction system for joining connecting a filiform element to a connection element thus conceived is susceptible to numerous modifications and variants, all coming under the scope
10 of the inventive concept; in addition, all details may be substituted by technically [[-]] equivalent elements. In practice, any materials of any size may be used, according to the requirements and to the state of the art.